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Towards an Elevated Temperature and Pressure 3-Electrode Hydrodynamic Channel Flow Cell

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Motivation & Overall Goal

- Fundamental electrocatalyst characterization at Elevated T&P
- Desired conditions: $P \ge 10 \ bar \rightarrow$ increased gas solubility (reactant or product); $T = 150 \circ C \rightarrow$ kinetic & selectivity effects
- Flexible electrolyte composition and real-time pH tuning

The Elevated T&P Channel Flow Cell (E-TP CFC) CNC-machined polyether-ether ketone (PEEK) Chemically & mechanically stable Internal (pseudo)reference electrode Interchangeable electrode discs



The Physical Electrochemistry of Channel Flow Cells

Hydrodynamic systems (alternative to rotating disc electrodes)^[1] \blacktriangleright The flowrate \dot{V} directly controls the mass transport and current I_{LIM} Submillimetric channel height $h_{ch} \rightarrow$ possible ohmic effects^[4] In Jaminar regimes. $k_{cell} = 1.467$

$$|I_{LIM}|^{[2]} = n_e - \cdot F \cdot k_{cell} \cdot C_{bulk} \left(\frac{A_{WE}^{geo} \cdot D}{h_{ch}}\right)^{2/3} \cdot \sqrt[3]{\dot{V}}$$

Finite-Element Simulations





 $D^{[3]} = 3.47 \cdot 10^{-6} \ cm^2 s^{-1}$

 $h_{ch} = 0.055 \ cm$

 $A_{WE}^{geo} = 0.196 \ cm^2$

Dummy Flow Cell Benchmarking at Room Temperature

 H_{UPD} on $Pt_{(poly)}$ Disc in H_2SO_4 0.5 M, v = 50 mV/s Hydrogen Underpotential Deposition <mark>ح</mark> 150 Correct potential sensing, little resistance \triangleright Potential values are independent on \dot{V} ► Traces of $O_{2(liq)}$ → negative current shift -300 -3.38 mL/min 1.2 1.4 **Limiting Current Analysis** 0.2 0.6 WE Potential vs. RHE, E [V] Fe^{III}(CN)₆]^{3−}+1e[−] → [Fe^{II}(CN)₆]^{4−}; $K_3Fe(CN)_6$ 10 mM + KNO₃ 0.2 M ▶ 0.05 → 1.6 V, v = 250 mV/s CVsPt & GC discs both work as WE (CE = GC) $|I_{LIM}|_{Calc} = 7.54 \cdot 10^{-4} \cdot \sqrt[3]{\dot{V}} \rightarrow \Delta_{Exp/Calc} = +12.9\%$ Literature \triangleright No disturbances, laminar flow (0.04 < Re < 114) **Data** [2] 10 mM [Fe^{III}(CN)₆]³⁻ Cathodic Scans vs. Flowrate 1.5 2.0 2.5 3.0 3.5 $U^{1/3} / (\mu L s^{-1})^{1/3}$ -0.01 mL/min 0.3 -0.10 mL/min $|\mathbf{I}_{\text{LIM}}|$ vs. (flowrate)^{1/3} —0.50 mL/min 0.15 7.5E-04 —1 mL/min y = 8.660E-04x-2 mL/min $6.0E-04 = R^2 = 9.989E-01$ —4 mL/min -6 mL/min -0.15 4.5E-04 -8 mL/min —10 mL/min **3.0E-04** —12 mL/min



Primary Current Distribution Over Circular Electrodes

Inhomogeneous current densities



References

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[4] Coles, B.A., Compton, R.G., Larsen, J.P., Spackman, R.A. Electroanalysis (1996), 8, No. 10

Conclusions & Future Perspectives

The DCFC demonstrated the effectiveness of the geometry and design Completing the commissioning and optimization of the E-TP CFC plant • Multiphysics modelling of P, T & V effects and comparison with experiments Benchmark tests at the E-TP conditions, then "real" catalyst studies

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